

The art of evaluating monitoring schemes – how to measure the performance of control charts?

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Synopsis

- 1. Notational Preliminaries.
- 2. Some history/drawbacks of performance measuring in SPC.
- 3. Concepts in detail.
- 4. Computational remarks.
- 5. Résumé.

The change-point model

Modeling of a stochastic process with a possible distributional change

Sequence of random variables $X_1, X_2, ...$ with cdf $\{F_{(i)}\}$ and a certain (unknown) time point m = change-point with

$$F_{(i)} = \begin{cases} F_0 & , i < m \\ F_1 & , i \ge m \end{cases}$$

Example: $F_0 = \mathcal{N}(\mu_0, 1)$, $F_1 = \mathcal{N}(\mu_1, 1)$ + independence

Notation: $\begin{cases} \{X_i\}_{i=1}^{m-1} & -\text{ process in control,} \\ \{X_i\}_{i=m}^{\infty} & -\text{ process out of control.} \end{cases}$

Control charts – SPC at work

different names, same concepts:

change point detection, continuous inspection, surveillance, monitoring ...

Aim: Detect rapidly and reliably, whether there appeared change-point m!

- ▶ Transformation $\{X_i\}_{i=1,2,...,n} \rightarrow Z_n$ and
- ▶ Stopping time $L = \min \{ n \in \mathbb{N} : Z_n \notin \mathcal{O} = [c_l^*, c_u^*] \}$,

At time point L observation is stopped & the scheme signals an **alarm**.

L is a random value on $\mathbb{N} = \{1, 2, 3, \ldots\}$.

Measuring control chart performance

- 1. Shewhart (192x, 193x) similar to tests: error probabilities,
- 2. Aroian/Levene (1950) average spacing number and average efficiency number,
- 3. GIRSHICK/RUBIN (1952) Bayesian framework,
- 4. PAGE (1954) introduced term ARL as the average number of articles inspected between to successive occasions when rectifying action is taken.
- 5. BARNARD (1959) If it were thought worthwile one could use methods analogous to these given by Page (1954) and estimate the average run length as a function of the departure from the target value. However, as I have already indicated, such computations could be regarded as having the function merely of avoiding unemployment amongst mathematicians.

Average Run Length (ARL)

Notation: $E_m(.)$ expectation for given change-point m.

Definition:

$$ARL = egin{cases} E_{\infty}(L) & , \ {
m process in \ control} \ E_1(L) & , \ {
m process \ out \ of \ control} \end{cases}$$

Note that for dealing with the ARL, the sequence $\{X_i\}$ is (strong) stationary with the same probability law for all *i*. Thus, e.g.,

$$ARL = E_{\mu}(L) =: \mathcal{L}_{\mu}.$$

Measuring control chart performance II

6. SHIRYAEV (1961/3) random change-point model

$$P(M=m) = egin{cases} \pi & , \ m=0 \ (1-\pi)\,(1-p)^{m-1}p & , \ m>0 \end{cases}, \ \pi\in [0,1)\,, \ p\in (0,1)$$

and minimize

$$\begin{cases} P_{\pi,p}(L < M) + c E_{\pi,p}(L - M)^+ & \text{for all s.t. } L\\ E_{\pi,p}(L - M | L \ge M) & \text{for all s.t. } L \text{ with } P_{\pi,p}(L < M) \le \alpha \end{cases}$$

 $m \ge 1$

7. ... 9.
$$E_{\infty}(L) \ge A$$

7. ROBERTS (1966) $\mathcal{D} := \lim_{m \to \infty} E_m (L - m + 1 | L \ge m)$
("steady-state ARL", R. "replaced" ∞ by 9)
8. LORDEN (1971) $\mathcal{W} := \sup_{m \ge 1} \text{ess sup } E_m ((L - m + 1)^+ | \mathcal{F}_{m-1})$
9. POLLAK/SIEGMUND (1975) $\mathcal{D}_{PS} := \sup_{m \ge 1} E_m (L - m + 1 | L \ge m)$

Anyway,

the ARL is the dominating measure!

Possible reasons:

Shewhart chart

$$\mathcal{W} = \mathcal{D} = \mathcal{D}_{\mathsf{PS}} = \mathcal{L} = E_1(L) = E_m(L - m + 1|L \ge m).$$

CUSUM

 $\mathcal{W}=\mathcal{D}_{\mathsf{PS}}=\mathcal{L}\text{,}$

modifications: $\mathcal{D}=\mathcal{D}_{\mathsf{PS}}\neq\mathcal{L}.$

But:

EWMA

All measures provide different values.

...

Lai 1995

Sequential changepoint detection in quality control and dynamical systems, J. R. Stat. Soc., Ser. B, 57, 613-658.

- ► The ARL constraint $E_{\theta_0}(T) \ge \gamma$ stipulates a long expected duration to false alarm. However, a large mean of T does not necessarily imply that the probability of having a false alarm before some specified time m is small. In fact, it is easy to construct positive integer-value random variables T with a large mean γ and also having a high probability that T = 1.
- In practice, the system only fails after a very long in-control period and we expect many false alarms before the first correct alarm. It is therefore much more relevant to consider
 - (a) the probability of no false alarm during a typical (steady state) segment of the base-line period and
 - (b) the expected delay in signaling a correct alarm,

instead of the ARL which is the mean duration to the first alarm assuming a constant in-control or out-of-control value.

${\rm Fris\acute{e}n}~2003$

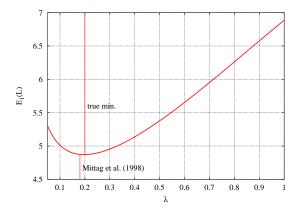
Statistical Surveillance. Optimality and Methods. *International Statistical Review*, **71**, *403-434*.

The whole subsection 3.5 (titled "ARL") is dedicated to a reckoning with "the criterion of minimal ARL".

For demonstrating the possible drawbacks of utilizing "the criterion of minimal ARL", let us consider one-sided EWMA- S^2 control charts, which resemble good candidates for illuminating this phenomenon.

One-sided EWMA- S^2 chart for monitoring variance

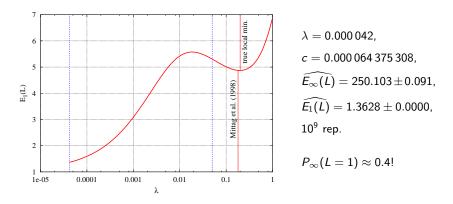
$$\begin{split} & Z_i = (1-\lambda)Z_{i-1} + \lambda S_i^2 \,, \ i \geq 1 \,, \ Z_0 = z_0 = \sigma_0^2 = 1 \,, \ S_i^2 = 1/4 \sum_{j=1}^5 (X_{ij} - \bar{X}_i)^2 \,, \\ & L = \inf \left\{ i \in \mathbb{N} \, : \, Z_i > \sigma_0^2 + c \sqrt{\lambda/(2-\lambda)} \sqrt{2/4} \, \sigma_0^2 \right\} \,, \\ & E_\infty(L) = 250 \,, \ \sigma_1^2 = 1.5^2 \quad \text{(as in Mittag et al., 1998)}. \end{split}$$



One-sided EWMA- S^2 chart for monitoring variance II

$$\begin{split} Z_i &= (1-\lambda)Z_{i-1} + \lambda S_i^2 \,, \ i \geq 1 \,, \ Z_0 = z_0 = \sigma_0^2 = 1 \,, \ S_i^2 = 1/4 \sum_{j=1}^{\infty} (X_{ij} - \bar{X}_i)^2 \,, \\ L &= \inf \left\{ i \in \mathbb{N} \,: Z_i > \sigma_0^2 + c \sqrt{\lambda/(2-\lambda)} \sqrt{2/4} \, \sigma_0^2 \right\} \,, \\ E_{\infty}(L) &= 250 \,, \ \sigma_1^2 = 1.5^2 \quad \text{(as in Mittag et al., 1998)}. \end{split}$$

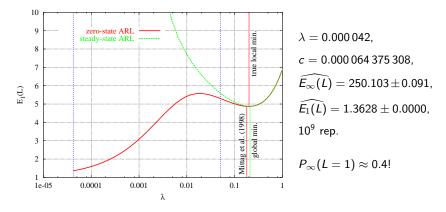
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One-sided EWMA- S^2 chart for monitoring variance III

$$\begin{aligned} Z_i &= (1-\lambda)Z_{i-1} + \lambda S_i^2 , \ i \ge 1 \ , \ Z_0 = z_0 = \sigma_0^2 = 1 \ , \ S_i^2 = 1/4 \sum_{j=1}^{5} (X_{ij} - \bar{X}_i)^2 \ , \\ L &= \inf \left\{ i \in \mathbb{N} : Z_i > \sigma_0^2 + c \sqrt{\lambda/(2-\lambda)} \sqrt{2/4} \ \sigma_0^2 \right\} \ , \\ E_{\infty}(L) &= 250 \ , \ \sigma_1^2 = 1.5^2 \quad (\text{as in Mittag et al., 1998}). \end{aligned}$$

5



Assessing the steady-state

$$\begin{aligned} \mathcal{F}_{m-1} &= \sigma \left(X_1, \dots, X_{m-1} \right), \ \mathcal{F}_{m-1}^* = \sigma \left(\mathcal{F}_{m-1} \cap \{ L > m-1 \} \right), \\ D_{(m)}^* &= E_m \left(L - m + 1 \, | \, \mathcal{F}_{m-1}^* \right) = \mathcal{L}_{\mu_1} (Z_{m-1}^*) \quad \text{for Markovian schemes}, \\ Z_{m-1}^* &\sim f_{m-1}^* (\cdot), \\ \psi_{\mu_0}(z) &= \lim_{m \to \infty} f_{m-1}^*(z) \qquad (\text{cf. to MADSON/CONN, 1973}), \\ D^* &= \mathcal{L}_{\mu_1}(Z^*), \ Z^* &\sim \psi_{\mu_0}(\cdot) \qquad \boxed{\text{name } D^* \text{ "steady-state delay"}}, \\ E(D^*) &= \int_{\mathcal{O}} \psi_{\mu_0}(z) \, \mathcal{L}_{\mu_1}(z) \, d\mathcal{M}(z) \\ &= \lim_{m \to \infty} \int_{\mathcal{O}} f_{m-1}^*(z) \, \mathcal{L}_{\mu_1}(z) \, d\mathcal{M}(z) = \mathcal{D} \quad (\text{steady-state ARL}) \\ &\approx E(D_{(m)}^*) = E_m \big(L - m + 1 \, | \, L \ge m \big) \quad \text{already for small } m. \end{aligned}$$

Links between D^* and previous measures

$$D_{(m)}^* = E_m (L - m + 1 | \mathcal{F}_{m-1}^*),$$

$$E_m ([L - m + 1]^+ | \mathcal{F}_{m-1}) = D_{(m)}^* \cdot I_{\{L > m-1\}} + 0 \cdot I_{\{L \le m-1\}},$$

$$\mathcal{W} = \sup_{m \ge 1} \operatorname{ess\,sup} (D_{(m)}^*) = \operatorname{ess\,sup} D^*,$$

$$\mathcal{D}_{\mathsf{PS}} = \sup_{m \ge 1} E(D_{(m)}^*).$$

 Z^* is random variable on \mathcal{O} with $z_0 \in \mathcal{O}$ and density $\psi_{\mu_0}(\cdot)$:

$$\begin{aligned} \mathsf{ARL} &= \mathcal{L}_{\mu_1}(z_0) \,, \\ \mathcal{W} &= \mathsf{ess}\,\mathsf{sup}\,\mathcal{L}_{\mu_1}(Z^*) \,, \\ \mathcal{D} &= \mathcal{E}\big(\mathcal{L}_{\mu_1}(Z^*)\big) \,, \\ \mathcal{D}_{\mathsf{PS}} &= \mathsf{max}\{\mathcal{L}_{\mu_1},\mathcal{D}\} \,. \end{aligned}$$

One-sided Schemes

► CUSUM: PAGE (1954)

$$\begin{aligned} &Z_n = \max \left\{ 0, Z_{n-1} + X_n - k \right\}, \ Z_0 = z_0 \,, \\ &L = \inf \left\{ n \in \mathbb{N} : Z_n > h \right\} \qquad \left(k = (\mu_0 + \mu_1)/2 \right) \end{aligned}$$

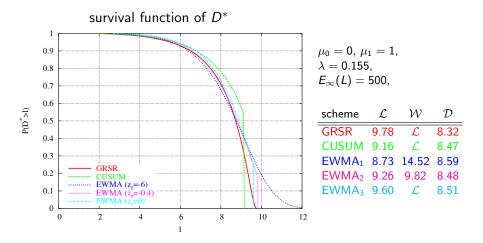
► EWMA: ROBERTS (1959) (reflecting barrier – WALDMANN (1986), GAN (1993))

$$Z_n = \max \left\{ z_{\text{reflect}}^*, (1 - \lambda) Z_{n-1} + \lambda X_n \right\}, \ Z_0 = z_0,$$
$$L = \inf \left\{ n \in \mathbb{N} : Z_n > c \sqrt{\lambda/(2 - \lambda)} \right\}, \ z_{\text{reflect}}^* = z_r \sqrt{\lambda/(2 - \lambda)}$$

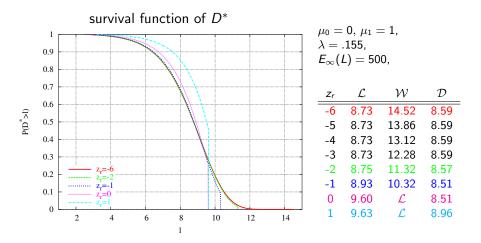
► GRSR: GIRSHICK/RUBIN (1952), SHIRYAEV (1963/76), ROBERTS (1966)

$$\begin{aligned} &Z_n = (1+Z_{n-1})\exp(X_n-k)\,, \ Z_0 = z_0\,, \\ &L = \inf \left\{ n \in \mathbb{N} \, : \, Z_n > g \right\} \qquad \qquad \left(\exp \left[(\mu_1 - \mu_0) \, X_n - (\mu_1^2 - \mu_0^2)/2 \right] \right) \end{aligned}$$

Dealing with D^* for one-sided schemes



Dealing with D^* for one-sided EWMA schemes



Two-sided Schemes

- CUSUM: coupling of 1-sided schemes
- CROSIER-CUSUM (1986)

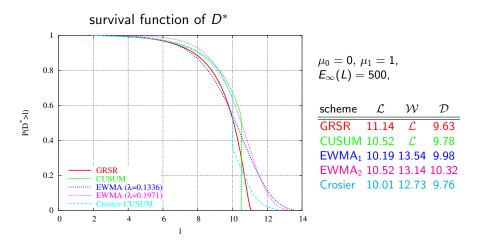
$$Z_{n} = \begin{cases} 0 & , \ C_{n} \leq k \\ (Z_{n-1} + X_{n}) \cdot \left(1 - \frac{k}{C_{n}}\right) & , \ C_{n} > k \end{cases}, \ C_{n} = |Z_{n-1} + X_{n}| \text{ for } n \geq 1,$$
$$L = \inf \{n \in \mathbb{N} : |Z_{n}| > h\}$$

► EWMA: ROBERTS (1959)

$$Z_n=(1-\lambda)\,Z_{n-1}+\lambda\,X_n\,,\,\,Z_0=z_0\,,\,\,L=\inf\left\{n\in\mathbb{N}\,:\,|Z_n|>c\,\sqrt{\lambda/(2-\lambda)}
ight\}$$

 GRSR: POLLAK/SIEGMUND (1985) - Z_n = (Z_n⁺ + Z_n⁻)/2 performs like coupling of 1-sided schemes Z_n = max{Z_n⁺, Z_n⁻} → coupling (PS: L_{μ1} = 11.142, E(D^{*}) = 9.644, coupling: L_{μ1} = 11.142, E(D^{*}) = 9.630, both: L_{μ0} = 500)

Dealing with D^* for two-sided schemes



α worst case ARL

Definition: $W_{\alpha} = \inf \{ w : P(D^* > w) \leq \alpha \}$

chart	shift Δ							measure
	0	0.5	1.0	1.5	2.0	2.5	3.0	measure
EWMA	689	39	10.0	5.1	3.4	2.6	2.2	L
	*	42	12	6.3	4.3	3.4	2.8	$W_{.05}$
	*	42	12	6.6	4.7	3.6	3.0	$W_{.01}$
	*	43	13	7.0	5.0	3.9	3.3	$W_{.001}$
	*	45	14	8.2	6.0	4.8	4.1	$\mathcal{W}_{<10^{-9}}$
CUSUM	724	34	9.9	5.6	3.9	3.1	2.6	\mathcal{L}/\mathcal{W}
GRSR	697	33	10.4	6.2	4.4	3.5	2.9	\mathcal{L}/\mathcal{W}

ROBERTS (1966) A comparison of some control chart procedures. *Technometrics*, **8**, 411-430.

 $\lambda = 0.25$, c = 2.87, one-sided, no reflexion (here reflected at $z_r = -6$)

Revisiting Mittag et al. (1998)

Their "winning" scheme is (for monitoring normal variance)

$$\begin{split} Z_i &= (1-\lambda)Z_{i-1} + \lambda S_i^2 \,, \ i \ge 1 \,, \ Z_0 = z_0 = \sigma_0^2 = 1 \,, \\ S_i^2 &= 1/4 \sum_{j=1}^5 (X_{ij} - \bar{X}_i)^2 \,, \\ L &= \inf \left\{ i \in \mathbb{N} : Z_i > \sigma_0^2 + c \sqrt{\lambda/(2-\lambda)} \sqrt{2/4} \, \sigma_0^2 \right\} \,, \\ E_\infty(L) &= 250 \,, \ \lambda = .18 \,, \ c = 2.91 \,. \end{split}$$

Revisiting Mittag et al. (1998) II

- Replace for EWMA-S² the original values λ and c by λ = 0.197 and c = 2.971.
- Remove the ln S² based and the S based schemes, and deploy CUSUM-S²:

$$Z_i = \max \left\{ 0, Z_{i-1} + S_i^2 - k
ight\}, \ i \ge 1 \ , \ Z_0 = z_0 = 0 \ ,$$

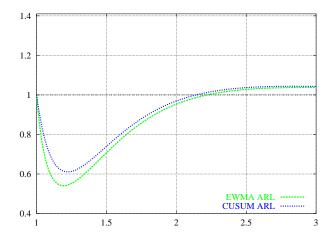
 $E_\infty(L) = 250 \ , \ k = 1.4597 \ , \ h = 3.117 \ .$

Determine as in Mittag et al. the efficiency

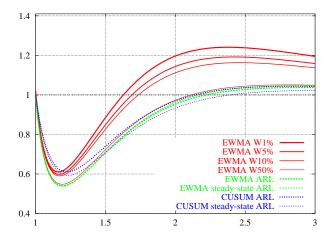
measure_{EWMA/CUSUM-S²}

measure_{Shewhart-S²}

Revisiting Mittag et al. (1998) III

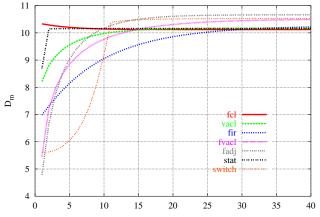


Revisiting Mittag et al. (1998) IV



Final advocacy for the steady-state ARL

 $D_m = E_m(L - m + 1 | L \ge m)$ vs. limit $E(D^*)$ (different EWMA charts with $\lambda = 0.1$, $E_{\infty}(L) = 500$, $\mu_1 = 1$)



m

Computational remarks

It seems so that fast accurate computation of

 $\mathcal{L}_{\mu}(z), \psi_{\mu}(z), P_{\infty}(L \leq n), P_{m}(L \leq n+m-1|L \geq m-1), \mathcal{D}$

is possible for univariate distributions which span to the whole real line (or at least they ensure smooth transition kernels over O).

 For univariate distributions restricted to the half real line or similar, collocation (might) provide the same for

 $\mathcal{L}_{\mu}(z), \psi_{\mu}(z), \mathcal{D}.$

- Exact results are available in only some cases.
- Monte-Carlo simulations are always possible. They demand, however, elaborate cpu time. Eventually, they are useful for validating of results.
- Mostly, the universal Markov chain approach provides suitable results, while programming efforts remain on a reasonable level.
- All become worse for multivariate distributions or dependent data.

Résumé

- Be cautious in applying the "minimal ARL criterion", especially in the one-sided case.
- Use the "steady-state ARL criterion". GRSR is asymptotically optimal in the one-sided case. The performance differences between the common schemes are practically negligible. Thus, look for the "steady-state ARL" optimal mode of your favorite scheme/chart.
- The pessimistic user has to apply the CUSUM scheme, which operates with probabilities of 10% and considerably more under worst case condition.
- Use the Markov chain approach in the first place as analysis tool. It provides all the information you need with sufficient accuracy and parsimonious expenditure of writing program code. Monte-Carlo simulations might complete your quantitative analysis.